

(12) **United States Patent**
Munson

(10) **Patent No.:** **US 9,476,399 B1**
(45) **Date of Patent:** **Oct. 25, 2016**

(54) **GLOW PLUG TYPE ACOUSTIC
RESONANCE IGNITER**

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(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 683 days.

(21) Appl. No.: **13/894,919**

(22) Filed: **May 15, 2013**

Related U.S. Application Data

(60) Provisional application No. 61/647,696, filed on May
16, 2012.

(51) **Int. Cl.**
F02P 23/00 (2006.01)
F02P 3/12 (2006.01)

(52) **U.S. Cl.**
CPC **F02P 23/00** (2013.01)

(58) **Field of Classification Search**
CPC F02K 9/76; F02K 9/766; F02K 9/78;
F02K 9/18; F02K 9/62; F02K 9/64; F02K
9/42; F02K 9/72; F02K 9/94; F02K 9/95;
F02C 7/26; F02C 7/264; F02P 23/00; F02P
3/12

See application file for complete search history.

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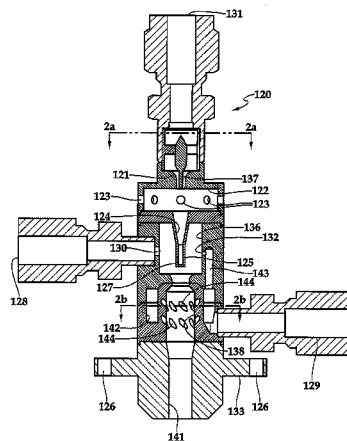
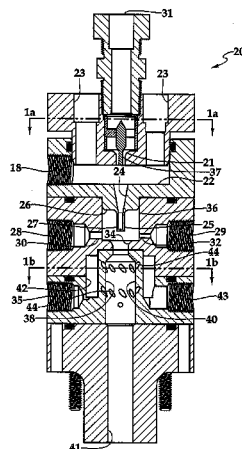
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(57) **ABSTRACT**

An acoustic resonance igniter uses high-pressure helium to
heat a resonance cavity so a hot surface of the resonance
cavity forms a source of ignition to a combustion chamber.
The resonance cavity may be round or may extend linearly
to increase the size of the hot surface. The combustion
chamber is cooled by arranging a feed of hydrogen and
oxygen which is oxygen rich and which becomes more so
when ignition occurs. A second combustion chamber
receives the combustion chamber output and adds additional
hydrogen through ports tangential to the wall of the second
combustion chamber to enrich the fuel ratio and cool the
second combustion chamber. The acoustic resonance igniter
is used to ignite a large rocket engine or to form a rocket
thruster.

20 Claims, 2 Drawing Sheets



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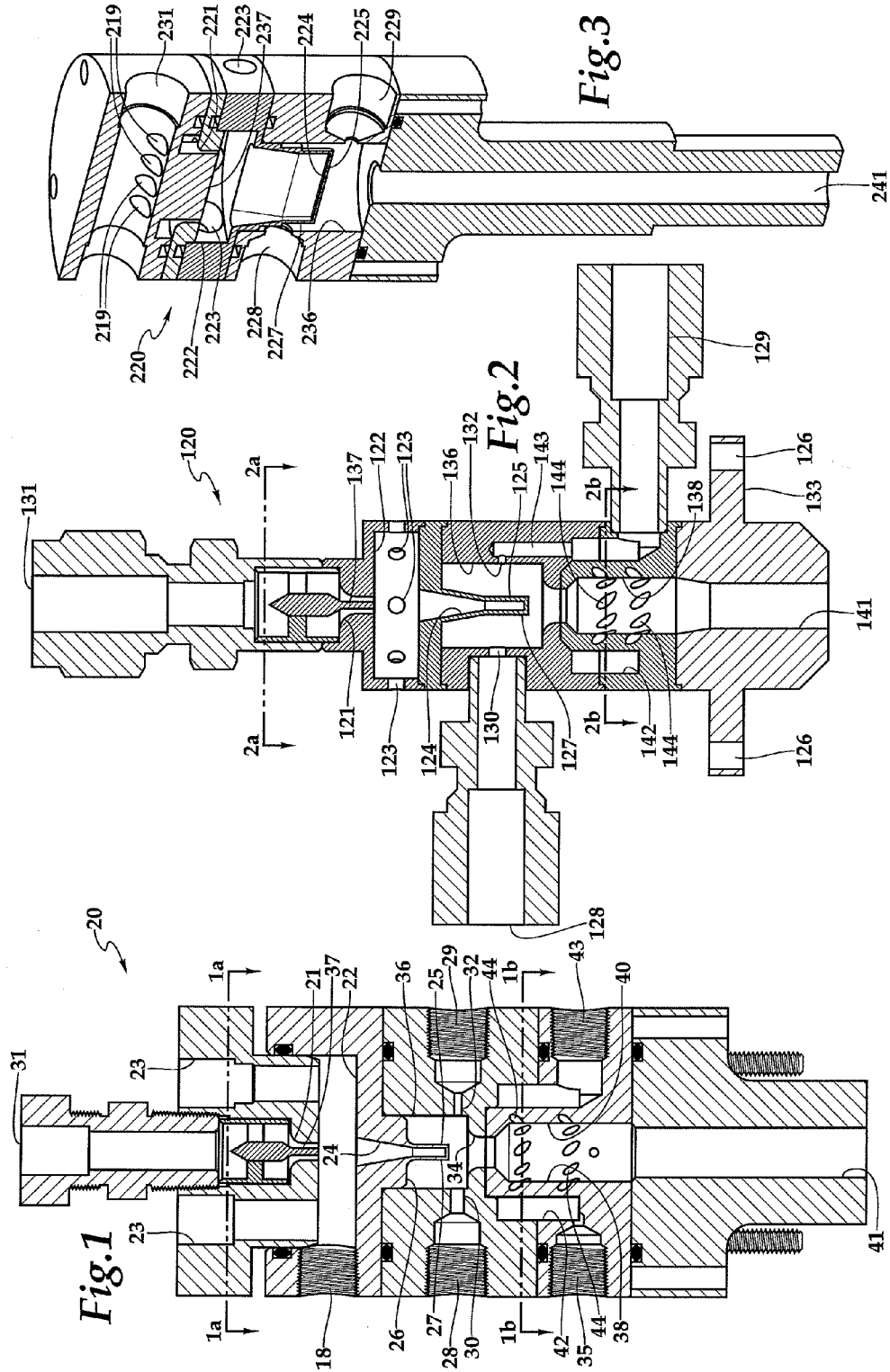
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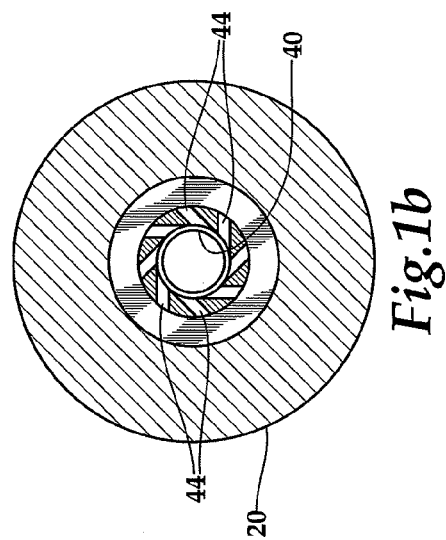
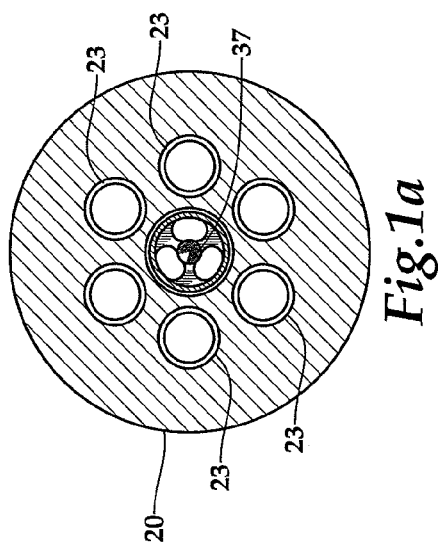
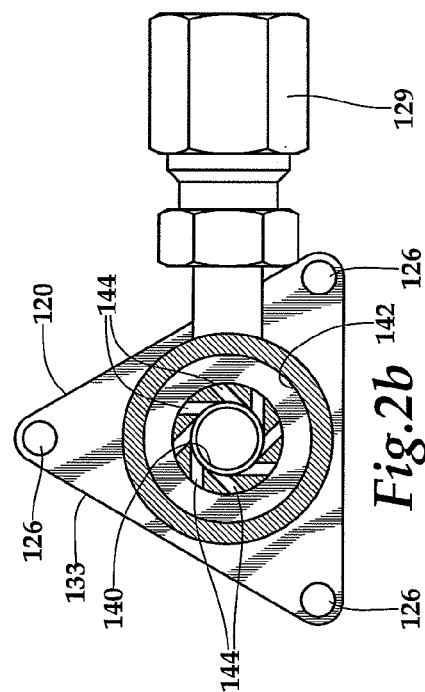
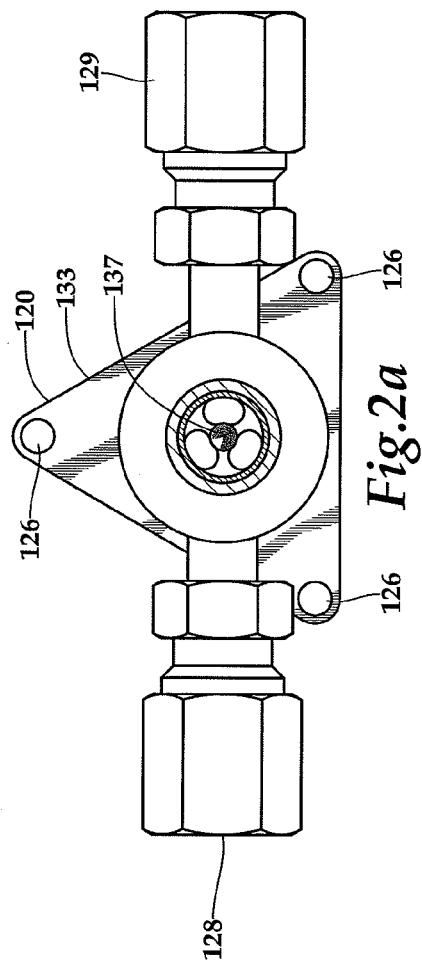
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**GLOW PLUG TYPE ACOUSTIC
RESONANCE IGNITER****CROSS REFERENCES TO RELATED
APPLICATIONS**

This application claims priority on U.S. Provisional Patent App. No. 61/647,696 Filed May 16, 2012, the disclosure of which is incorporated by reference herein.

**STATEMENT AS TO RIGHTS TO INVENTIONS
MADE UNDER FEDERALLY SPONSORED
RESEARCH AND DEVELOPMENT**

This invention was made with government support under contract to US Air Force Research Laboratory # FA9300-10-C-2105. The government has certain rights in the invention. The government may exercise such rights over assignee's objection in accordance with 35 U.S.C. 202 and 203 if the government finds such action necessary in accord with 35 U.S.C. 203(a)(1-4).

BACKGROUND OF THE INVENTION

The present invention relates to igniters such as are used in rocket engines, jet engines and combustors in general; and to igniters utilizing a hot surface, heated by acoustically heated gas, as an ignition source in particular.

Generally the safest, most reliable and most widely used method of igniting a combustor which does not employ a pilot light is an electrical spark. This approach is generally reliable and safe, e.g., such as used in an internal combustion engine spark plug. Historically, however, igniters for rocket engines have often used a pyrotechnic igniter or hypergolic ignition to assure reliable engine ignition. Ignition is particularly a concern in liquid rocket engines where both the fuel and oxidizer are supplied as liquids to the chamber, because any momentary delay in ignition can result in the accumulation of an explosive mixture of fuel and oxidizer, resulting in a hard start which may damage or destroy the engine. Restartable rocket engines are often necessary where the engine is used to perform orbit circularization, orbital maneuvers, or orbital transfer. Multiple pyrotechnic igniters, one for each use of the engine, have been used. Reusable engines also require multiple starts, and, while replaceable pyrotechnic igniters are possible, they may leave residues which may add to the cost of reconditioning the engine for re-flight. Another approach to reliable ignition is to use propellants which are hypergolic (ignite on contact with each other) so that multiple restarts of the engine are not generally a problem. Hypergolic fuel combinations are widely used in rocket engines employed in missiles, rocket boosters, and/or maneuvering engines, in large part because they provide a simple and reliable ignition process. Non-hypergolic propellant combinations in rocket booster stages often use a limited quantity or slug of hypergolic propellant in one or both of the propellant lines or are separately injected into the combustion chamber to initiate combustion. In such a case multiple starts become complicated. Although engines utilizing hypergolic propellants readily perform multiple restarts and are widely used, using hypergolic propellant combinations limits propellant choice and can limit performance. Moreover, generally hypergolic propellants are themselves expensive and toxic, such that the cost of procurement and handling may be significantly increased as compared to non-hypergolic propellants.

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Electric spark ignition has been used to overcome these problems particularly with the hydrogen and oxygen propellant combination such as on the Pratt & Whitney RL 10 engine. Hydrogen and oxygen are clean burning, require low ignition energy, and have wide flammability limits. However, electrical ignition sources add complexity, require electrical power and a high-voltage electrical source, and are susceptible to electromagnetic damage such as caused by lightning strikes, and generally provide low ignition energy.

One possible ignition source which has been considered particularly for hydrogen and oxygen propellants is an acoustic igniter. An acoustic igniter employs a nozzle which directs an under-expanded sonic or supersonic gas jet into an essentially blind hole which forms an acoustic resonance tube. This arrangement, originally used as a high frequency noise source, was subsequently investigated as a simple way of obtaining a small quantity of very hot gas, or a hot surface which can be used as a source of ignition.

What is needed is a practical acoustic resonance igniter for H_2 and O_2 , particularly with relatively low pressure gasses.

SUMMARY OF THE INVENTION

The acoustic resonance igniter of this invention uses a high-pressure driver gas to heat a resonance cavity to a high temperature so the hot surface of the resonance cavity acts in the manner of a glow plug. An oxygen manifold supplies a primary combustion chamber of oxygen at a first regulated pressure, and hydrogen is supplied to the combustion chamber by a hydrogen manifold at a second regulated pressure which is lower than the oxygen manifold pressure. The primary combustion chamber exhausts through an exhaust orifice into a secondary combustion chamber, such that the pressure in the primary combustion chamber is governed by the pressure of the primary oxygen manifold, the size of the oxygen inlet port to the primary combustion chamber, and a manifold pressure of the primary hydrogen manifold and the size of the hydrogen inlet port to the primary combustion chamber, and finally by the size of the exhaust port orifice.

The primary hydrogen manifold and inlet port and the primary oxygen manifold and inlet port are arranged such that they have a high oxygen/fuel mixture ratio, for example 33, which is near the minimum energy for ignition of hydrogen and oxygen. The manifolds and the inlets are further arranged such that combustion in the primary combustion chamber drives the mixture ratio to a higher mixture ratio, for example 100, so that the combustion gases temperature reduce or eliminate the need for cooling of the primary combustion chamber. The highly oxygen rich combustion gases exit the primary combustion chamber through the exhaust orifice into the secondary combustion chamber where the temperature of the combustion gases is raised by the injection of additional hydrogen through the hydrogen manifold. The manifold forms an annulus around the secondary chamber and has inlet ports which are drilled at an angle, as shown in FIG. 1, so that the secondary hydrogen enters the combustion chamber through injection ports which are arranged to inject the hydrogen tangentially to the inside cylindrical wall of the secondary combustion chamber.

Operation in a typical sequence is by starting helium flowing through the sonic nozzle and into the resonance cavity, after which the helium is exhausted out through one or more exhaust ports. After some short interval of heating, the exterior of the resonance cavity will be in excess of 1500° K (1230° C., 2246° F.), well above the autoignition

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temperature for H₂ and O₂ gas. After the short heating interval, the main propellant valves are opened, first H₂ then O₂. Under cold-flow conditions, the mixture ratio in the primary combustion chamber is approximately 33, which is near the mixture ratio (O/F) of minimum ignition energy. Once combustion occurs in the primary chamber, a pressure drop will occur across the primary chamber throat and the mixture ratio in the region adjacent to the resonance cavity will rise to approximately 100. This mixture ratio will result in a much cooler flame temperature in the primary combustion chamber, thus enhancing the hardware survivability. In the secondary combustion chamber, the secondary hydrogen will be injected to trim out the mixture ratio to an O/F of approximately 1.5. Additionally, this secondary fuel is injected in a swirling pattern to provide film cooling to the rest of the igniter and transfer tube.

It is a feature of the invention to provide for ignition of low-pressure hydrogen and oxygen with high-pressure helium in a glow plug type acoustic resonance igniter.

Further objects, features and advantages of the invention will be apparent from the following detailed description when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a front elevational cross-sectional view of a test configuration of the ignitor of this invention.

FIG. 1a is a cross-sectional view of the apparatus of FIG. 1 taken along line 1a-1a.

FIG. 1b is a cross-sectional view of the apparatus of FIG. 1 taken along line 1b-1b.

FIG. 2 is a front elevational cross-sectional view of a flight weight configuration of the ignitor of this invention.

FIG. 2a is a cross-sectional view of the apparatus of FIG. 2 taken along line 2a-2a.

FIG. 2b is a cross-sectional view of the apparatus of FIG. 2 taken along line 2b-2b.

FIG. 3 is a cut-away isometric view of an alternative embodiment of the ignitor of this invention, where a linear nozzle and linear resonance cavity are employed.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring more particularly to FIGS. 1-3, wherein like numbers refer to similar parts, a glow plug type acoustic resonance igniter 20 is shown in FIG. 1. The igniter 20 of FIG. 1 is a laboratory test article. A flight weight igniter 120 is shown in FIG. 2, and an alternative embodiment linear igniter 220 is shown in FIG. 3.

The resonance igniter 20 shown in FIG. 1 employs a high-pressure helium source 31, for example helium at 200-620 psia, which is accelerated through a sonic nozzle 21 into a lower pressure chamber 22 at, for example, 60 psia. A pintle 37 is mounted in the nozzle 21 to improve flow characteristics. A pressure test port 18 is shown in FIG. 1 for measuring pressure in the lower pressure chamber 22. The pressure in the lower pressure chamber 22 is maintained by outlets 23. The outlets form choked flow nozzles, whose outflows depend only upon the helium temperature and pressure but not on the external pressure to which the helium outlets 23 exhaust. Opposite the sonic nozzle 21 is a resonance cavity 24 similar to that described in U.S. application Ser. No. 13/396,919, filed on Feb. 15, 2012, which is incorporated herein by reference.

As described therein the resonance cavity 24 is arranged so that a sonic resonance wave is set up in the cavity which

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results in heating of the helium gas, particularly in the lowermost cylindrical portion 27 of the cavity. The resonance cavity 24 is shown as formed in part of a structural component 26 which also defines the lower portion of the pressure chamber 22. One possible material for forming the resonance cavity 24 is a molybdenum alloy such as TZM Molybdenum ASTM B386 type 364 (Alloy Plate, Sheet, Strip, and Foil) and B387 type 364 (Alloy Bar, Rod, and Wire) an alloy of 0.50% Titanium, 0.08% Zirconium and 0.02% Carbon with the balance Molybdenum.

After some short interval of heating, the exterior of the resonance cavity 24, i.e., the hot surface 25, will be in excess of 1500° K (1230° C., 2246° F.), well above the autoignition temperature for H₂ and O₂ gas. The inlet manifold for oxygen 28 and the inlet manifold for hydrogen 29 are arranged with manifold pressures and the inlet orifices 30, 32 together with the exhaust orifice, and flow channel 34 such that the primary combustion chamber 36 has a high oxidizer rich mixture ratio, for example 33:1, which is near optimal, i.e., minimum energy for ignition from the hot surface 25 of the surrounding lower cylindrical portion 27 of the resonance cavity. The arrangement of manifold pressures and orifice sizes are preferably arranged such that when the oxygen and hydrogen ignite, increasing the volume of the gases in the primary combustion chamber 36, the mixture ratio becomes, with or without active control, even more oxygen-rich, for example 100:1, so as to minimize heating in the primary combustion chamber 36 and the exhaust orifice 34. The exhaust orifice 34 does not generally operate with a choked flow (i.e., does not operate such that downstream conditions do affect the pressure in the primary combustion chamber).

To increase the flame temperature of the combustion gases from the primary combustion chamber 36, secondary hydrogen from an inlet 35 is added to the combustion gases in a secondary combustion chamber 38 into which the exhaust orifice 34 empties. Sufficient hydrogen to substantially lower the mixture ratio, for example to produce a mixture ratio of 1.5:1, is used to increase the energy of the combustion gases to produce a suitable torch for igniting the combustion chamber of a larger engine. To raise the energy of the combustion gases without overheating the walls 40 of the secondary combustion chamber, the secondary hydrogen gas from an inlet 43 is introduced through an annular manifold 42 which surrounds the secondary combustion chamber walls 40. The annular manifold 42 introduction is arranged so as to cool the secondary combustion chamber walls 40. The cooling injection the secondary combustion chamber walls 40 is arranged through ports 44 which are drilled through the chamber walls 40, best shown in FIG. 1b between the annular manifold 42 and the secondary combustion chamber, so that rows of holes, i.e., injection ports 44, enter the secondary combustion chamber at tangents to the inner cylindrical wall 40 of the combustion chamber and downwardly at a 45° angle with respect to an axis defined by the cylindrical chamber wall 40. The secondary hydrogen enters along the wall 40 of the combustion chamber 38 so as to induce rotation of the injected hydrogen to produce a shield of hydrogen gas around the secondary combustion chamber wall 40, and the transfer tube 41 to the larger oxygen-hydrogen engine (not shown).

The acoustic resonance igniters 20, 120 are configured to provide positive mixture ratio control during and after the ignition transient, either passively through the selection of the regulated gas pressures and orifices 30, 32, 130, 132 or actively by varying gas pressures and flows.

The "glow plug"-style resonance cavity device, i.e., the resonance cavity **24**, is located inside a primary combustion chamber **36** which is located upstream of a secondary combustion chamber **38**. All the oxidizer and a portion of the fuel is injected into the primary combustion chamber **36**. The primary propellants flow from the primary combustion chamber **36** through an unchoked orifice **34** into the secondary combustion chamber **38** where the balance of the fuel is injected. The propellant manifolds are kept at constant pressure through the use of pressure regulators in the propellant feed systems upstream of the igniter i.e., the hot surface **25**. The orifice between the primary **36** and secondary **38** combustion chambers serves to create a differential injection back pressure between the primary fuel injector and the secondary fuel injector. Prior to ignition, the mixture ratio (O/F) of the primary combustion chamber is approximately 30:1-40:1 (which is easily ignitable) and the mixture ratio of the secondary combustion chamber is approximately 1.0:1-1.2:1. After ignition, the pressure in both combustion chambers increases and the pressure drop through the inter-chamber orifice **34** increases as well. The post-ignition mixture ratio in the primary combustion chamber is approximately 100:1-120:1 (which results in a cooler flame temperature) and the mixture ratio in the secondary combustion chamber is approximately 1.4:1-1.6:1 resulting in a higher flame temperature. The igniter exhaust nozzle **41** exhausts to a near-vacuum prior to ignition. After ignition, the igniter exhausts into a rocket engine main combustion chamber that reaches pressures of up to 2000 psia. As the main combustion chamber pressure is elevated, the igniter manifold pressures are elevated accordingly, stopping the flow of gas to the primary **36** and secondary **38** combustion chambers. With ignition of the engine the flow of helium hydrogen and oxygen to the plug type acoustic resonance igniter **20** is shut down

The major sub-scale operating parameters of the acoustic resonance igniter illustrated and described with respect to FIG. **1** are listed in the table below:

| | Pre-Ignition | Post-Ignition | |
|---|--------------|---------------|----------------------|
| Oxygen Injector | | | |
| Oxygen Manifold Inlet Area | 0.0254 | 0.0254 | in ² |
| Oxygen Manifold Pressure | 40 | 40 | psia |
| Oxygen Injector Diameter | 0.076 | 0.076 | in |
| Oxygen Mass Flow Rate | 0.00460 | 0.00320 | lb _m /sec |
| Hydrogen Injectors | | | |
| Hydrogen Manifold Pressure | 30 | 30 | psia |
| Primary H ₂ Injector Diameter | 0.033 | 0.033 | in |
| Primary H ₂ Injector Flow Rate | 0.00014 | 0.00003 | lb _m /sec |
| Hydrogen Trim Injector Diameter | 0.041 | 0.041 | in |
| Hydrogen Trim Injector Num. | 16 | 16 | — |
| Hydrogen Trim Flow Rate | 0.00402 | 0.00216 | lb _m /sec |
| Primary Chamber | | | |
| Primary Mixture Ratio | 33 | 101 | — |
| Primary Chamber Temperature | 300 | 1620 | K |
| Primary Chamber Pressure | 18.7 | 30.0 | psia |
| Primary Chamber Throat Diameter | 0.15 | 0.15 | in |
| Primary Chamber Throat Area | 0.0177 | 0.0177 | in ² |
| Primary Mass Flow Rate | 0.00474 | 0.00323 | lb _m /sec |
| Primary Chamber Throat ΔP | 4.8 | 4.7 | psid |
| Secondary Chamber | | | |
| Global Mixture Ratio | 1.1 | 1.5 | — |
| Global C* | N/A | 8213 | ft/sec |
| Global T _{Ad} | 300 | 1668 | K |
| Total Mass Flow Rate | 0.00876 | 0.00540 | lb _m /sec |
| Secondary Chamber Pressure | 13.8 | 26.3 | psia |

-continued

| | Pre-Ignition | Post-Ignition | |
|------------------------|--------------|---------------|-----------------|
| Nozzle | | | |
| Nozzle Throat Diameter | 0.258 | 0.258 | in |
| Nozzle Throat Area | 0.0523 | 0.0523 | in ² |

A flight weight arrangement of the plug type acoustical resonance igniter **120**, is shown in FIG. **2**. The primary differences over the igniter **20** is the use of braze joints for assembly to reduce weight, and the use of a single gas hydrogen inlet **129** which connects to the hydrogen manifold **142** which in turn is connected through a passageway **143** and an orifice **132**, which feeds the primary combustion chamber **136**. The gaseous oxygen source **128** at about 30 psi is supplied to the primary combustion chamber **136** through an inlet orifice **130**. The igniter **120** has cooling injection holes **144**, and combustion gases exhaust through nozzle **141**.

An additional feature is that helium exhaust outlets **123** are arranged to exit radially from a lower pressure chamber **122** through which helium exits, the outlets **123** form a plurality of choked flow exhaust outlets in the igniter **120**.

The flight weight arrangement of the plug type acoustical resonance igniter **120** incorporates, a helium inlet **131**, and hot surface **125** of a lower cylindrical part **127** of the resonance cavity **124**. The resonance igniter **120** also has a mounting flange **133** with three holes **126** for receiving mounting fasteners (not shown) which mount the igniter **120** to a combustion chamber (not shown).

Ignition of hydrogen and oxygen requires a certain amount of the heated gases to reach the autoignition temperature. In such a situation the temperature of the hot surface, the area of the hot surface, and the velocity of the gases passing by the hot surface will all affect the ability and speed at which the hot surface igniter ignites the gases.

Shown in FIG. **3** is an acoustic resonance igniter **220** arranged to increase the size of the heated surface **225** by arranging a resonance cavity **224** which extends linearly a selected distance e.g., 0.080 to 1.000 inches, across a primary combustion chamber **236**. The linear extension forms resonance cavities **224** for example of 0.040"×0.500" up to 0.080"×1.000". The liner resonance cavity **224** is fed by a linear jet of helium. The linear jet of helium is formed by helium from the inlet **231** at a pressure of about 200-620 psia which feeds a plurality of inlets **219** on both sides of a linear pintle **237**, centered in a linear sonic nozzle **221**. The pintle is similar to the pintles **37**, **137** but is linearly extended as shown in FIG. **3**. The helium exhaust outlets **223** are arranged to exit radially from a lower pressure chamber **222** through which helium exits. The outlets **223** form a plurality of choked flow exhaust outlets in the igniter **220**. The Helium from the manifold **131** as it passes through the linear sonic nozzle **221** forms a linearly extending sonic jet of helium. The linearly extending sonic jet of helium sets up resonance within the linear resonance cavity **224**, which is positioned along a plane defined by the linear extension of the linear sonic nozzle **221**. The resonance within the linear resonance cavity **224** heats the linear lower portion of the resonance cavity **227** to from a linearly extending hot ignition surface **225**.

The primary combustion chamber **236** contains the hot surface **225**, and, because of the larger hot surface, a larger quantity of hydrogen and oxygen gas can be fed to the primary chamber from gaseous oxygen inlet **228** and gas-

eous hydrogen inlet **229**. This may eliminate the necessity of the secondary chamber **236** to increase the temperature or adjust the mixture ratio of the gases, which may be used directly to ignite a larger rocket engine combustion chamber. Alternatively the secondary combustion chamber **236** such as shown in FIGS. **1** and **2** can be used.

Although the acoustic resonance igniter has been described for use with gaseous hydrogen and oxygen, other propellants could be used, whether liquid or gas, including bipropellants and monopropellants including those described in U.S. application Ser. No. 13/396,919.

It should be understood that the resonance cavity **24**, **124**, **224** could be formed of a separate thin-walled structure. Such a thin-walled structure is formed of a high temperature thermally conductive material resistant to hot hydrogen, oxygen and hydroxyl vapor, such as the molybdenum alloy TZM Molybdenum ASTM B386 type 364.

It should be understood that the pintles **37**, **137**, **237** in the linear sonic nozzle **21**, **121**, **221** of the igniters **20**, **120**, **220** shown in FIGS. **1-3** could be omitted so long as a sonic jet of helium or other suitable low molecular weight gas is formed.

It should be understood that a larger area of the hot surface, and the resulting greater contact time of the propellant gases e.g., hydrogen and oxygen, over the hot surface can result in faster ignition or can support the ignition of larger flows of propellant gases or both.

It should be understood that the acoustic resonance igniter of this invention is most effective with a lightweight molecular monatomic gas such as helium as the resonance gas. A lightweight diatomic gas such as hydrogen is also very effective. Heavier monatomic gases such as neon, argon, and krypton or heavier diatomic gases such as nitrogen and oxygen could also be effective sources of ignition depending on the temperature needed. In this regard, although the invention has been described as using high temperature to achieve reliable and fast ignition, use of a catalytic surface, such as platinum on the heated surface of the lowermost portion of the cavity, could be used in combination with a lower temperature. Use of catalyzers may not be preferred because of the problem of catalyst contamination and the associated quality control issues of determining that an active catalyst surface is present when the igniter is called upon to function.

It should be understood that a linear pintle in the sonic nozzle is not strictly necessary, although without a linear pintle the flow rates of helium may be greater or the effectiveness of the heating in the resonance chamber may be less.

It should be understood that the essentially blind resonance cavity may have an opening from which hot gas escapes without preventing the operation of the resonance cavity described above if the opening is sufficiently small. However, such an opening is not necessary in the embodiments shown in the figures.

It is understood that the invention is not limited to the particular construction and arrangement of parts herein illustrated and described, but embraces all such modified forms thereof as come within the scope of the following claims.

I claim:

1. A hot surface acoustic resonance igniter comprising: a source of compressed gas having a molecular weight of about 2 to 4;
- a sonic gas nozzle defining an opening and a nozzle axis, the gas nozzle connected to the source of compressed gas;

a structure supported with respect to the gas nozzle, wherein portions of the structure define a cavity which is configured to form a resonance cavity having an opening in the upper surface which is spaced from the gas nozzle along the nozzle axis, the structure forming a lower surface of the resonance cavity, which is arranged to be heated by gas from the source of compressed gas which is driven to resonate by being emitted from the sonic nozzle;

a primary combustion chamber defined below the lower surface of the resonance cavity, the primary combustion chamber connected to a source of propellant;

a secondary combustion chamber separated from the primary combustion chamber by a flow channel, the secondary combustion chamber in combustion gas receiving relation to the primary combustion chamber, the secondary combustion chamber having an elongated chamber wall along which combustion products flow; and

portions of the combustion chamber elongated chamber wall forming secondary propellant injection ports, arranged at least in part tangential to the chamber wall to form a cooling layer of propellant along the combustion chamber wall.

2. The resonance igniter of claim **1** wherein the structure supported with respect to the gas nozzle is comprised of a support component, and mounted thereto a resonance cavity forming structure.

3. The resonance igniter of claim **1** wherein the source of compressed gas is a source of helium.

4. The resonance igniter of claim **3** wherein the source of helium is a source of 200 to 620 psi helium.

5. The resonance igniter of claim **1** further comprising an annular manifold connected to the source of propellant, the annular manifold surrounding at least part of the secondary combustion chamber elongated chamber wall along which combustion products flow;

wherein the secondary propellant injection ports connect the annular manifold to the combustion chamber.

6. The resonance igniter of claim **5** further comprising a passageway which connects the annular manifold to an orifice which feeds into the primary combustion chamber.

7. The resonance igniter of claim **5** wherein the secondary combustion chamber elongated chamber wall has portions defining a cylinder having an inner cylindrical wall and a cylinder axis; and

wherein the secondary propellant injection ports are positioned in the portions defining the cylinder, and the secondary propellant injection ports are at least partially tangential to the inner cylindrical wall.

8. The resonance igniter of claim **7** wherein the secondary propellant injection ports are tangent to the inner cylindrical wall angled downwardly at about a 45° angle with respect to the cylinder axis.

9. The resonance igniter of claim **1** wherein the primary combustion chamber is connected to two sources of propellant comprising an oxidizer source and a fuel source.

10. The resonance igniter of claim **9** wherein the oxidizer source is a source of gaseous oxygen at a selected pressure and the fuel source is a source of gaseous hydrogen at a selected pressure.

11. The resonance igniter of claim **10** wherein the source of gaseous oxygen is connected through a first orifice of a first selected area to the primary combustion chamber, and the source of gaseous hydrogen is connected through a second orifice of a second selected area to the primary combustion chamber, and wherein the first orifice selected

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area, the gaseous oxygen source pressure, the second orifice selected area, and the gaseous hydrogen source pressure, are selected so that a mixture ratio of weight of oxygen to weight of hydrogen in the primary combustion chamber is 30-40 to 1, and that when the gaseous oxygen and the gaseous hydrogen are ignited the mixture ratio of weight of oxygen to weight of hydrogen increases.

12. The resonance igniter of claim 1 further comprising a pintle extending into the nozzle opening.

13. A hot surface acoustic linear resonance igniter comprising:

a source of compressed hydrogen or helium gas;
a linearly extending sonic gas nozzle defining a linearly extending nozzle opening, and a nozzle plane centered on the linearly extending opening of the sonic gas nozzle;

wherein the gas nozzle is connected to the source of compressed hydrogen or helium gas, to form a linear gas jet which extends along the nozzle plane;

a structure, portions of the structure forming an upper surface, a linearly extending resonance opening and a linearly extending resonance cavity extending away from the linear opening, the linear opening supported spaced from the linearly extending sonic gas nozzle so that the linear opening and the linearly extending resonance cavity extend linearly in the nozzle plane;

wherein the structure has a lower linear surface external to the resonance cavity and opposite the resonance cavity, which lower surface is arranged to be heated by a resonance produced by the linear gas jet emitted by the linearly extending sonic gas nozzle; and

a combustion chamber defined below the lower surface of the resonance cavity, the combustion chamber connected to a source of propellant.

14. The resonance igniter of claim 13 wherein the nozzle opening, the resonance opening and the resonance cavity extend linearly about 0.25 to 1.0 inches.

15. The resonance igniter of claim 13 further comprising a linearly extending pintle extending into the nozzle opening.

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16. The resonance igniter of claim 15 wherein the source of compressed hydrogen or helium gas is connected to a manifold with a plurality of inlets which connect the source of hydrogen or helium compressed gas to the linearly extending sonic gas nozzle.

17. The resonance igniter of claim 13 further comprising:

a secondary combustion chamber separated from the combustion chamber by a flow channel, the secondary combustion chamber in combustion gas receiving relation to the combustion chamber, the secondary combustion chamber having an elongated chamber wall along which combustion products flow; and

portions of the elongated chamber wall forming secondary propellant injection ports, arranged at least in part tangential to the combustion chamber wall to form a cooling layer of propellant along the combustion chamber wall.

18. The resonance igniter of claim 13 wherein the combustion chamber is connected to two sources of propellant comprising: an oxidizer source and a fuel source.

19. The resonance igniter of claim 18 wherein the oxidizer source is a source of gaseous oxygen at a selected pressure and the fuel source is a source of gaseous hydrogen at a selected pressure.

20. The resonance igniter of claim 19 wherein the source of gaseous oxygen is connected through a first orifice of a first selected area to the combustion chamber, and the source of gaseous hydrogen is connected through a second orifice of a second selected area to the combustion chamber, and wherein: the first orifice selected area, the gaseous oxygen source pressure, the second orifice selected area, and the gaseous hydrogen source pressure, are selected so that a mixture ratio of weight of oxygen to weight of hydrogen in the combustion chamber is 30-10 to 1, and that when the gaseous oxygen and the gaseous hydrogen are ignited the mixture ratio of weight of oxygen to weight of hydrogen increases.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 9,476,399 B1
APPLICATION NO. : 13/894919
DATED : October 25, 2016
INVENTOR(S) : Scott M. Munson

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Claims

Column 10, Line 34, "the combustion chamber is 30-10 to 1" should be -- the combustion chamber is 30-40 to 1 --.

Signed and Sealed this
Third Day of January, 2017

A handwritten signature in black ink, reading "Michelle K. Lee". The signature is fluid and cursive, with the first letters of each name being capitalized and prominent.

Michelle K. Lee
Director of the United States Patent and Trademark Office